

# Entropy Stable Residual Distribution Method

## Scalar Equation

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# The Fundamental of Entropy Control

## Main Concept

### Entropy Control

Positivity

Order of Accuracy

Limiter

Blending

There are three keywords here:

- Entropy Conservation: The entropy will not be increased or decreased.
- Entropy Stability: The entropy will always be generated with physical (correct) sign.
- Entropy Consistency: The entropy will always be generated with physical (correct) sign and amount.



# The Fundamental of Entropy Control

## Main Concept

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Consider a new signal distribution for RD methods,

$$\phi_i = \frac{1}{2} ((f_i, g_i) - (f^*, g^*)) \cdot \vec{n}_i$$

The entropy conservation enforce that,

$$\sum_i v_i^T \phi_i = \frac{1}{2} \sum_i (F_i, G_i) \cdot \vec{n}_i$$

Or,

$$\sum_i (v_i^T (f_i, g_i) \cdot \vec{n}_i) - (f^*, g^*) \sum_i (v_i^T \vec{n}_i) = \sum_i (F_i, G_i) \cdot \vec{n}_i$$



# New RD Proposal

## Signal Distribution

### Entropy Control

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We propose an artificial terms which alters the signals distribution in the following form.

$$\phi_i = \frac{1}{2} ((f_i, g_i) - (f^*, g^*)) \cdot \vec{n}_i \\ - \alpha(\mathbf{v}_j - \mathbf{v}_i) - \beta(\mathbf{v}_k - \mathbf{v}_i) - \gamma(\mathbf{v}_i - \mathbf{v}_k)$$

where  $(j, k)$  are the neighboring points to node  $i$  and that are to be determined.



# New RD Proposal

## The Entropy Generation

### Entropy Control

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$$\begin{aligned}\dot{U} &= \frac{1}{2} \sum_i (F_i, G_i) \cdot \vec{n}_i - \frac{1}{2} \sum_i v_i^T (f_i, g_i) \cdot \vec{n}_i \\ &\quad + \frac{1}{2} (f^*, g^*) \sum_i (v_i^T \vec{n}_i) \\ &\quad + \sum_i v_i^T (\alpha(v_j - v_i) + \beta(v_k - v_j) + \gamma(v_i - v_k)) \\ &= - \sum_i v_i^T (\alpha(v_i - v_j) + \beta(v_j - v_k) + \gamma(v_k - v_i)) \\ &= - \frac{\alpha - \gamma}{2} ((v_1 - v_2)^2 + (v_2 - v_3)^2 + (v_3 - v_1)^2) \\ &\quad - \beta(v_1 v_2 - v_2 v_1 + v_2 v_3 - v_3 v_2 + v_3 v_1 - v_1 v_3) \leq 0 \\ &\alpha > \gamma, \quad \forall \beta \rightarrow \alpha > 0, \quad \gamma = -\alpha, \quad \forall \beta\end{aligned}$$



# N-scheme Recovery

Determined  $\alpha$  and  $\beta$

Entropy Control

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$$\alpha = \begin{cases} \frac{2([\mathbf{v}]_{ji} + [\mathbf{v}]_{ki})\phi_T}{3([\mathbf{v}]_{ij}^2 + [\mathbf{v}]_{jk}^2 + [\mathbf{v}]_{ki}^2)} & \text{Two-Target} \\ \frac{2\phi_T(4v_i + v_j + v_k) - 3(k_i v_i^2 + k_j v_j^2 + k_k v_k^2)}{3([\mathbf{v}]_{ij}^2 + [\mathbf{v}]_{jk}^2 + [\mathbf{v}]_{ki}^2)} & \text{One-Target} \end{cases}$$
$$\beta = \begin{cases} \frac{k_j - k_k}{6} + \frac{k_j[\mathbf{v}]_{jk}^2 - k_k[\mathbf{v}]_{ij}^2}{[\mathbf{v}]_{ij}^2 + [\mathbf{v}]_{jk}^2 + [\mathbf{v}]_{ki}^2} & \text{Two-Target} \\ \left(\frac{k_j - k_k}{6}\right) \left(\frac{6[\mathbf{v}]_{jk}^2}{[\mathbf{v}]_{ij}^2 + [\mathbf{v}]_{jk}^2 + [\mathbf{v}]_{ki}^2} - 1\right) & \text{One-Target} \end{cases}$$



# N-scheme Recovery

## Signals

Entropy Control

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N-scheme will be recovered as follow,

$$\begin{array}{l} \text{Two-Target} \\ k_i < 0, \quad k_j, k_k > 0, \end{array} \quad \left\{ \begin{array}{l} \tilde{\phi}_i^N = 0 \\ \tilde{\phi}_j^N = k_j^+(u_j - u_i) \\ \tilde{\phi}_k^N = k_k^+(u_k - u_i) \end{array} \right.$$
  
$$\begin{array}{l} \text{One-Target} \\ k_i > 0, \quad k_j, k_k < 0, \end{array} \quad \left\{ \begin{array}{l} \tilde{\phi}_i^N = k_i u_i + k_j u_j + k_k u_k \\ \tilde{\phi}_j^N = 0 \\ \tilde{\phi}_k^N = 0 \end{array} \right.$$



# Linearized Approach

## Simplified

Entropy Control

Positivity

Order of Accuracy

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In order to simplify the formulation for  $\alpha$  and  $\beta$ , define,

$$\delta_{i,j,k} = v_{i,j,k} - \bar{v}$$

Therefore,

$$v_j = v_i + \delta_k + 2\delta_j, \quad v_k = v_i + 2\delta_k + \delta_j$$

Assuming  $\delta_j \simeq \delta_k$ ,

Method	$\alpha$	$\beta$
Lax-Friedrichs	$\frac{1}{6} (k_k + k_j + 2k_{\max})$	$\frac{1}{6} (k_k - k_j)$
N (two-target)	$\frac{1}{3} (k_j + k_k)$	$\frac{1}{3} (k_j - k_k)$
LDA (two-target)	$\frac{1}{3} (k_j + k_k)$	$\frac{1}{3} (k_j - k_k)$
One-Target	$-\frac{1}{6} (k_j + k_k)$	$-\frac{1}{6} (k_j - k_k)$





# Positivity Check

General  $\alpha$  and  $\beta$

Entropy Control

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Recall the linear signal distribution,

$$\begin{cases} \tilde{\phi}_i = \frac{1}{3}k_i([u]_{ij} - [u]_{ki}) - \alpha([u]_{ji} - [u]_{ik}) - \beta[u]_{kj} \\ \tilde{\phi}_j = \frac{1}{3}k_j([u]_{jk} - [u]_{ij}) - \alpha([u]_{kj} - [u]_{ji}) - \beta[u]_{ik} \\ \tilde{\phi}_k = \frac{1}{3}k_k([u]_{ki} - [u]_{jk}) - \alpha([u]_{ik} - [u]_{kj}) - \beta[u]_{ji} \end{cases}$$

Simplifying,

$$\begin{cases} \tilde{\phi}_i = \left(\frac{2}{3}k_i + 2\alpha\right) u_i + \left(-\frac{1}{3}k_i - \alpha + \beta\right) u_j + \left(-\frac{1}{3}k_i - \alpha - \beta\right) u_k \\ \tilde{\phi}_j = \left(-\frac{1}{3}k_j - \alpha - \beta\right) u_i + \left(\frac{2}{3}k_j + 2\alpha\right) u_j + \left(-\frac{1}{3}k_j - \alpha + \beta\right) u_k \\ \tilde{\phi}_k = \left(-\frac{1}{3}k_k - \alpha + \beta\right) u_i + \left(-\frac{1}{3}k_k - \alpha - \beta\right) u_j + \left(\frac{2}{3}k_k + 2\alpha\right) u_k \end{cases}$$

Thus, the positivity condition will be,

$$\alpha > -\frac{1}{3}k_{\min}, \quad |\beta| < \alpha + \frac{1}{3}k_{\min} \quad (1)$$



# Order of Accuracy

Isotropic Grid

Entropy Control

Positivity

Order of Accuracy

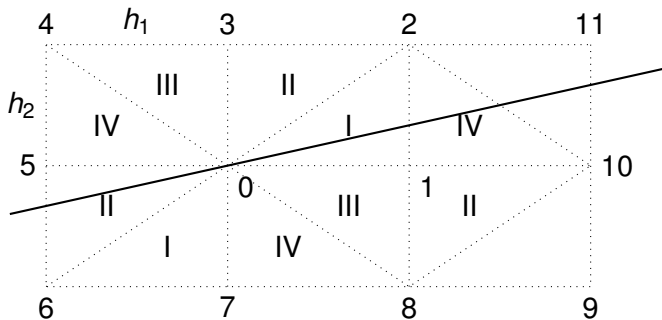
Limiter

Blending

$$TE = TE^{\text{iso}} + TE^{\text{art}} = O(h^3) + TE^{\text{art}}$$

The geometrical dimensions are ( $h_1 = h, h_2 = hs$ ).  
Assume,

$$\alpha = \tilde{\alpha}h, \quad \beta = \tilde{\beta}h, \quad \gamma = \tilde{\gamma}h$$



# Order of Accuracy

## Isotropic Grid

Entropy Control

Positivity

Order of Accuracy

Limiter

Blending

There are four types of triangle (I, II, III, VI). For each type  $\alpha$ ,  $\beta$  and  $\gamma$  are same. Thus, the truncation error is,

$$\begin{aligned} TE = & \left( - \left( \tilde{\alpha}_I + \tilde{\alpha}_{II} + \tilde{\alpha}_{III} + \tilde{\alpha}_{IV} - \tilde{\gamma}_I - \tilde{\gamma}_{II} - \tilde{\gamma}_{III} - \tilde{\gamma}_{IV} \right) a^2 s^2 \right. \\ & + \left( 2\tilde{\alpha}_I - \tilde{\alpha}_{III} - \tilde{\alpha}_{IV} - \tilde{\beta}_I + \tilde{\beta}_{II} - \tilde{\beta}_{III} + \tilde{\beta}_{IV} - \tilde{\gamma}_I - \tilde{\gamma}_{II} + 2\tilde{\gamma}_{III} \right) abs \\ & - \left( \tilde{\alpha}_I + \tilde{\alpha}_{II} + 2\tilde{\alpha}_{IV} - \tilde{\beta}_I + \tilde{\beta}_{II} + \tilde{\beta}_{III} - \tilde{\beta}_{IV} - 2\tilde{\gamma}_{II} - \tilde{\gamma}_{III} - \tilde{\gamma}_{IV} \right) b^2 \left( \frac{u_{nn}}{2r^2 s} \right) h \\ & + \left( 2b^3 \left( \tilde{\alpha}_{IV} + \tilde{\beta}_{II} - \tilde{\beta}_{IV} - \tilde{\gamma}_{II} \right) + ab^2 s \left( \tilde{\alpha}_{III} - \tilde{\alpha}_{IV} - \tilde{\beta}_I + \tilde{\beta}_{II} - \tilde{\beta}_{III} + \tilde{\beta}_{IV} + \tilde{\gamma}_I - \tilde{\gamma}_{II} \right) \right. \\ & \left. + a^2 bs^2 \left( 2\tilde{\alpha}_{II} + \tilde{\alpha}_{III} - \tilde{\alpha}_{IV} + \tilde{\beta}_I - 3\tilde{\beta}_{II} - \tilde{\beta}_{III} + 3\tilde{\beta}_{IV} - \tilde{\gamma}_I + \tilde{\gamma}_{II} - 2\tilde{\gamma}_{IV} \right) \right) \left( \frac{u_{nnn}}{4r^3 s} \right) h^2 \\ & + O(h^3) \end{aligned}$$

High order way,

$$\alpha, \beta, \gamma = O(h^q) \Rightarrow \text{Order of Accuracy} = q + 1$$



# Minmod Limiter

## Basis

Entropy Control

Positivity

Order of Accuracy

Limiter

Blending

Minmod limiter could be applied as,

$$\Omega_i^{\text{LMT}} = \frac{\max(0, \Omega_i)}{\sum_p \max(0, \Omega_p)}, \quad \Omega_i = \frac{\phi_i}{\phi_T}$$

And,

$$\phi_i^{\text{LMT}} = \Omega_i^{\text{LMT}} \phi_T$$

This limiter could implement on the N and Lax-Friedrichs approaches. There are three possibilities for the  $\Omega_{i,j,k}$ :

$$\Omega_{i,j,k} \geq 0, \quad \Omega_i < 0, \Omega_{j,k} \geq 0, \quad \Omega_i \geq 0, \Omega_{j,k} < 0.$$



# Signal Limiter For $\alpha$ and $\beta$

All Positive

Entropy Control

Positivity

Order of Accuracy

Limiter

Blending

All positive,  $\Omega_i, \Omega_j, \Omega_k \geq 0$  which is going back to the original signal distribution. Because the LP is satisfied in this condition automatically.

$$\Omega_{i,j,k} = \frac{\phi_{i,j,k}}{\phi_T}$$



# Signal Limiter For $\alpha$ and $\beta$

## Two Positive

Two positive,  $\Omega_i < 0$  and  $\Omega_j, \Omega_k \geq 0$  which leads to,

$$\begin{cases} \tilde{\phi}_i^{\text{LMT}} = (1 - p)\tilde{\phi}_i \\ \tilde{\phi}_j^{\text{LMT}} = \tilde{\phi}_j + p\tilde{\phi}_i\Omega_j^{\text{LMT}} \\ \tilde{\phi}_k^{\text{LMT}} = \tilde{\phi}_k + p\tilde{\phi}_i\Omega_k^{\text{LMT}} \end{cases}, \quad 0 \leq p \leq 1, \quad \Omega_j^{\text{LMT}} + \Omega_k^{\text{LMT}} = 1$$

For  $p = 1$  the limiter will reduce to the classic minmod.

$$\begin{cases} \tilde{\phi}_i = \left(\frac{2}{3}k_i + 2\alpha\right) u_i + \left(-\frac{1}{3}k_i - \alpha + \beta\right) u_j + \left(-\frac{1}{3}k_i - \alpha - \beta\right) u_k \\ \tilde{\phi}_j = \left(-\frac{1}{3}k_j - \alpha - \beta\right) u_i + \left(\frac{2}{3}k_j + 2\alpha\right) u_j + \left(-\frac{1}{3}k_j - \alpha + \beta\right) u_k \\ \tilde{\phi}_k = \left(-\frac{1}{3}k_k - \alpha + \beta\right) u_i + \left(-\frac{1}{3}k_k - \alpha - \beta\right) u_j + \left(\frac{2}{3}k_k + 2\alpha\right) u_k \end{cases}$$

which leads to,

$$p < \min \left[ \frac{\frac{1}{3}k_j + \alpha + \beta}{\Omega_j^{\text{LMT}} \left(\frac{2}{3}k_j + 2\alpha\right)}, \frac{\frac{2}{3}k_j + 2\alpha}{\Omega_j^{\text{LMT}} \left(\frac{1}{3}k_j + \alpha - \beta\right)}, \frac{\frac{1}{3}k_k + \alpha - \beta}{\Omega_k^{\text{LMT}} \left(\frac{2}{3}k_k + 2\alpha\right)}, \frac{\frac{2}{3}k_k + 2\alpha}{\Omega_k^{\text{LMT}} \left(\frac{1}{3}k_k + \alpha + \beta\right)} \right]$$



# Signal Limiter For $\alpha$ and $\beta$

One Positive

One positive,  $\Omega_j, \Omega_k < 0$  and  $\Omega_i \geq 0$  that make the whole signal distribution one target after limiting,

$$\begin{cases} \tilde{\phi}_i^{\text{LMT}} = \tilde{\phi}_i + p(\tilde{\phi}_j + \tilde{\phi}_k) \\ \tilde{\phi}_j^{\text{LMT}} = (1-p)\tilde{\phi}_j \\ \tilde{\phi}_k^{\text{LMT}} = (1-p)\tilde{\phi}_k \end{cases}, \quad 0 \leq p \leq 1$$

Note that,  $p = 1$  for one positive case. Therefore,

$$\begin{cases} p < \frac{\frac{2}{3}k_i + 2\alpha}{-\frac{1}{3}k_i + 2\alpha} \\ p < \frac{\alpha - \beta + \frac{1}{3}k_i}{\alpha - \beta + k_j + \frac{1}{3}k_i}, & \alpha - \beta + k_j + \frac{1}{3}k_i > 0 \\ p < \frac{\alpha + \beta + \frac{1}{3}k_i}{\alpha + \beta + k_k + \frac{1}{3}k_i}, & \alpha + \beta + k_k + \frac{1}{3}k_i > 0 \end{cases}$$



# Blending Approach

## Main Idea

Entropy Control

Positivity

Order of Accuracy

Limiter

Blending

Recall,

$$\alpha, \beta, \gamma = O(h^q) \Rightarrow \text{Order of Accuracy} = q + 1$$

Consider,

$$\alpha = O(h^q) = -\gamma, \quad \beta = 0$$

For first order we use  $q = q_{\min} = 0$  and for high order  $q = q_{\max} = 1, 2, 3, \dots$ . Therefore, by changing the  $q$  the blending approach will be constructed.

$$\alpha = \psi h^{q_{\min}} + (1 - \psi) h^{q_{\max}}$$





# Blending Approach

## Sensor Definition

Entropy Control

Positivity

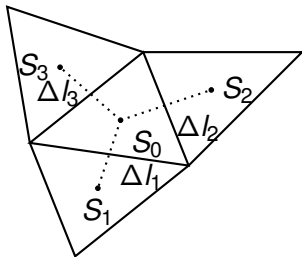
Order of Accuracy

Limiter

Blending

$$m_i^S = \left| \frac{S_i - S_0}{\Delta I_i} \right|, \quad m_{\max}^S = \max(m_1^S, m_2^S, m_3^S)$$

$$\psi = \begin{cases} 1 & m_{\max}^S \geq 1 \\ m_{\max}^S & m_{\max}^S < 1 \end{cases}$$



# Blending Approach

## Expansion

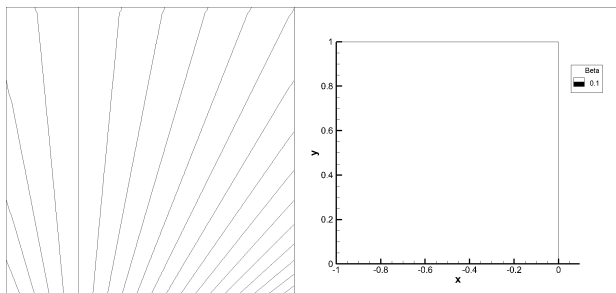
Entropy Control

Positivity

Order of Accuracy

Limiter

Blending



(a) Solution

(b) Sensor



# Blending Approach

## Tree

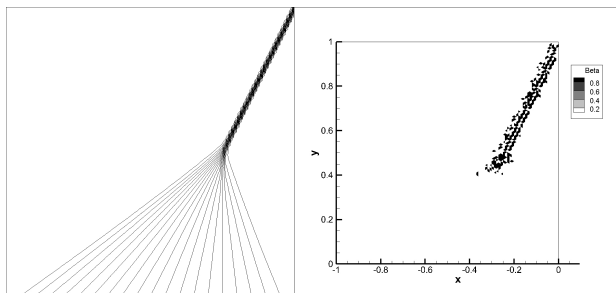
Entropy Control

Positivity

Order of Accuracy

Limiter

**Blending**



(c) Solution

(d) Sensor



Thank You



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