

# *Third-Order-Accurate for Scalar Conservation Laws*

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# Contents

- Divergence Theorem
- Numerical Integration
  - Trapezoidal Rule
  - Simpson's Rule
- Numerical Results
- Truncation Errors Analysis

# Divergence Theorem

3D : Divergence Theorem

2D : Green-Gauss Theorem

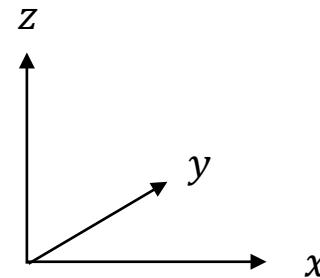
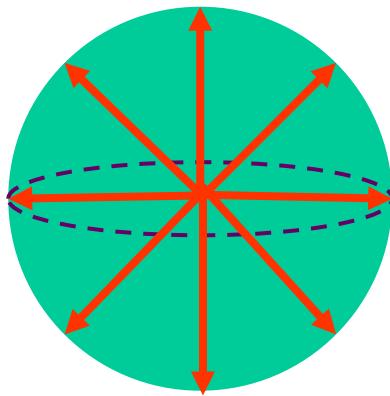
Examples to demonstrate the integration of flux-divergence using Green's theorem

# Divergence Theorem

In 3-D case: **Divergence Theorem**

$$\iiint_V \nabla \cdot \vec{F} \, dx \, dy \, dz = \iint_A \vec{F} \cdot \hat{n} \, dx \, dy$$

Divergence inside a volume  $V$  = fluxes that penetrate the bounded surface  $A$



## In 2-D case: Normal Form of Green's Theorem

$$\iint_S \nabla \cdot \vec{F} \, dx \, dy = \oint_{\partial S} \vec{F} \cdot \hat{n} \, dl$$

or commonly written in most textbooks as:

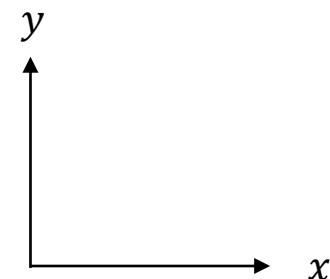
Let

$$\vec{F} = M \hat{i} + N \hat{j}$$

$$\nabla \cdot \vec{F} = \frac{\partial M}{\partial x} + \frac{\partial N}{\partial y}$$

Therefore,

$$\begin{aligned} \iint_S \left( \frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} \right) dx \, dy &= \oint_{\partial S} \vec{F} \cdot \hat{n} \, dl \\ &= \oint_{\partial S} M \, dy - N \, dx \end{aligned}$$



This is commonly known as **Green's theorem**.

# Examples of Exact Integration

Let us demonstrate the exact integration of flux-divergence in 2D.

**Divergence Theorem**

$$\iint_S \nabla \cdot \vec{F} dx dy = \oint_{\partial S} \vec{F} \cdot \hat{n} dl$$

**Scalar Conservation Law**

$$\frac{\partial u}{\partial t} + \nabla \cdot \vec{F}(u) = 0$$

## Problem statement

For the simplest case:

$$u(x, y) = x^2 + y^2 \quad \vec{\lambda} = (a_x, a_y)^T$$

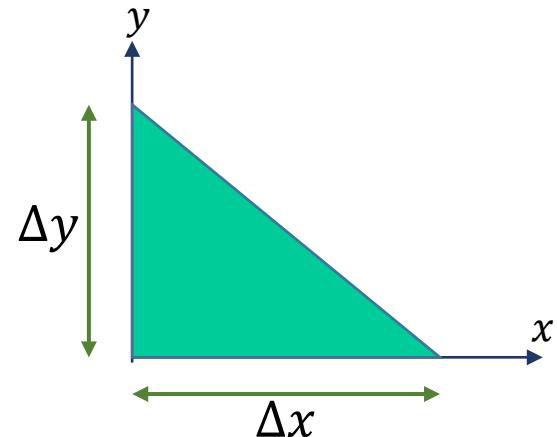
and the flux is

$$\vec{F}(u) = u \vec{\lambda}$$

Evaluate

$$\iint_S \nabla \cdot \vec{F} dx dy$$

where



Method 1:  $\iint_S \nabla \cdot \vec{F} dx dy = \oint_{\partial S} \vec{F} \cdot \hat{n} dl$

$$\nabla \cdot \vec{F}(u) = 2x + 2y$$

$$\int_{x=0}^{\Delta x} \int_{y=0}^{\Delta y - \frac{\Delta y}{\Delta x}x} (2x + 2y) dy dx$$

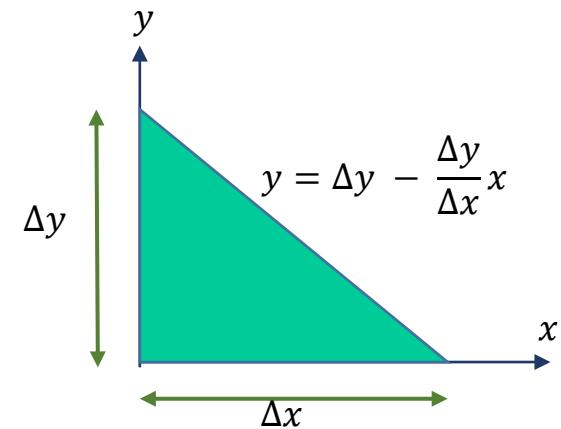
$$= \int_{x=0}^{\Delta x} [2xy + y^2]_{y=0}^{\Delta y - \frac{\Delta y}{\Delta x}x} dx$$

$$= \int_{x=0}^{\Delta x} \left[ 2x \left( \Delta y - \frac{\Delta y}{\Delta x}x \right) + \left( \Delta y - \frac{\Delta y}{\Delta x}x \right)^2 \right] dx$$

$$= \int_{x=0}^{\Delta x} \left[ 2x \left( \Delta y - \frac{\Delta y}{\Delta x}x \right) + \left( \Delta y - \frac{\Delta y}{\Delta x}x \right)^2 \right] dx$$

$$= \int_{x=0}^{\Delta x} \left[ \Delta y^2 + \left( 2\Delta y - 2\frac{\Delta y^2}{\Delta x} \right)x + \left( \frac{\Delta y^2}{\Delta x^2} - 2\frac{\Delta y}{\Delta x} \right)x^2 \right] dx$$

$$= \left[ x\Delta y^2 + \left( \Delta y - \frac{\Delta y^2}{\Delta x} \right)x^2 + \frac{1}{3} \left( \frac{\Delta y^2}{\Delta x^2} - 2\frac{\Delta y}{\Delta x} \right)x^3 \right]_{x=0}^{\Delta x} = \frac{1}{3}\Delta y^2\Delta x + \frac{1}{3}\Delta y\Delta x^2$$



**Method 1:**  $\iint_S \nabla \cdot \vec{F} dx dy = \oint_{\partial S} \vec{F} \cdot \hat{n} dl$

$$\vec{F}(u) = (x^2 + y^2)\hat{i} + (x^2 + y^2)\hat{j}$$

$$= \int_{l_{23}} \vec{F} \cdot \hat{n}_{23} dl + \int_{l_{31}} \vec{F} \cdot \hat{n}_{31} dl + \int_{l_{12}} \vec{F} \cdot \hat{n}_{12} dl$$

To perform the line integral, curves have to be expressed in parametric forms:

$$l_{23} \rightarrow \vec{r}(t) = \underbrace{(1-t)\Delta x}_{x} \hat{i} + \underbrace{t\Delta y}_{y} \hat{j} \quad 0 \leq t \leq 1$$

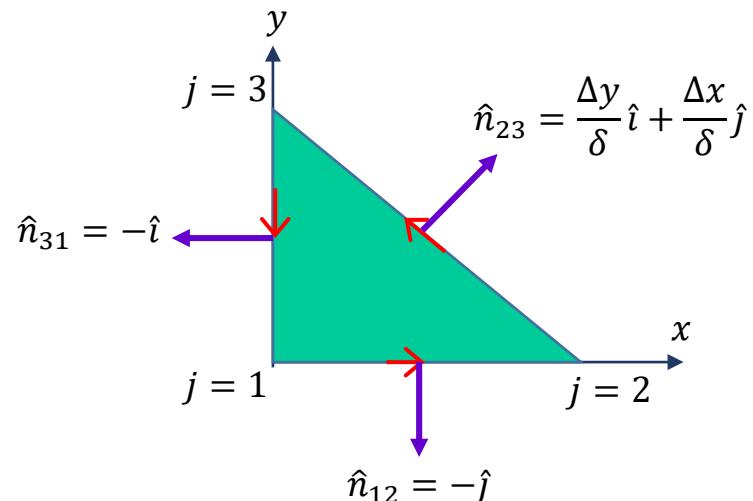
$$l_{31} \rightarrow \vec{r}(t) = \underbrace{0}_{x} \hat{i} + \underbrace{(1-t)\Delta y}_{y} \hat{j} \quad 0 \leq t \leq 1$$

$$l_{12} \rightarrow \vec{r}(t) = \underbrace{t\Delta x}_{x} \hat{i} + \underbrace{0}_{y} \hat{j} \quad 0 \leq t \leq 1$$

using the line integral of parametric equations:

Say  $\vec{F} \cdot \hat{n} = f(x(t), y(t))$   $\vec{r}(t) = x(t)\hat{i} + y(t)\hat{j}$

$$\int_{\vec{r}(t)} \vec{F} \cdot \hat{n} dl = \int_{t=0}^{t=1} f(x(t), y(t)) |\vec{v}(t)| dt$$



$$|\vec{v}(t)| = \sqrt{\left(\frac{\partial x(t)}{\partial t}\right)^2 + \left(\frac{\partial y(t)}{\partial t}\right)^2}$$

$$= \left[ \int_{l_{23}} \frac{\Delta y}{\delta} (x^2 + y^2) + \frac{\Delta x}{\delta} (x^2 + y^2) dl \right] - \int_{l_{31}} (x^2 + y^2) dl - \int_{l_{12}} (x^2 + y^2) dl$$

$$\int_{t=0}^{t=1} \left[ \frac{\Delta y}{\delta} (x^2 + y^2) + \frac{\Delta x}{\delta} (x^2 + y^2) \right] \delta dt$$

$$= (\Delta x + \Delta y) \int_{t=0}^{t=1} \left[ ((1-t) \Delta x)^2 + (t \Delta y)^2 \right] dt$$

$$= \frac{1}{3} (\Delta x^3 + \Delta x \Delta y^2 + \Delta y \Delta x^2 + \Delta y^3)$$

$$-\Delta y \int_{t=0}^{t=1} (1-t)^2 \Delta y^2 dt = -\frac{1}{3} \Delta y^3$$

$$-\Delta x \int_{t=0}^{t=1} t^2 \Delta x^2 dt = -\frac{1}{3} \Delta x^3$$

$$\therefore \int_{l_{23}} \vec{F} \cdot \hat{n}_{23} dl + \int_{l_{31}} \vec{F} \cdot \hat{n}_{31} dl + \int_{l_{12}} \vec{F} \cdot \hat{n}_{12} dl = \frac{1}{3} \Delta y^2 \Delta x + \frac{1}{3} \Delta y \Delta x^2$$

This result agrees with the calculation by doing the volume integration of the flux divergence directly.

# Numerical Integration

To connect the application of Green's theorem in  
RD method

# Numerical Integration

## Steady State:

The conditions for *second-order-accurate* are:

- 1) The integration of the flux-divergence must be third-order-accurate.

$$\iint_S \nabla \cdot \vec{F} \, dx \, dy = \oint_{\partial S} \vec{F} \cdot \hat{\vec{n}}_{ext} \, dl = - \oint_{\partial S} \vec{F} \cdot d\vec{n} = 0 + O(h^3)$$

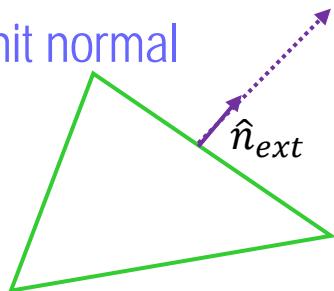
- 2) The distribution coefficient must be bounded.

$$0 \leq \beta_i^T \leq 1 \quad \Longrightarrow \quad \text{Linear-preserving scheme}$$

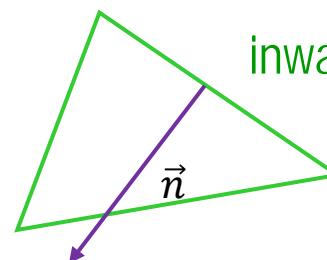
eg. LDA

## Remarks:

outward unit normal



inward scaled normal



The conditions for *third-order-accurate* are:

- 1) The integration of the flux-divergence must be fourth-order-accurate.

$$\iint_S \nabla \cdot \vec{F} dx dy = \oint_{\partial S} \vec{F} \cdot \hat{n}_{ext} dl = - \oint_{\partial S} \vec{F} \cdot d\vec{n} = 0 + O(h^4)$$

- 2) The distribution coefficient must be bounded.

$$0 \leq \beta_i^T \leq 1$$

## INTEGRATION OF FLUX-DIVERGENCE

In RD method, flux residual is defined as

$$\phi^T = \iint_S \nabla \cdot \vec{F} dx dy = \oint_{\partial S} \vec{F} \cdot \hat{n}_{ext} dl = - \oint_{\partial S} \vec{F} \cdot d\vec{n}$$

Integrate the flux crossing the 3 edges

**Trapezoidal Rule** *Second-Order-Accurate*

$$\phi^T = + \sum_{j \in T} k_j u_j$$

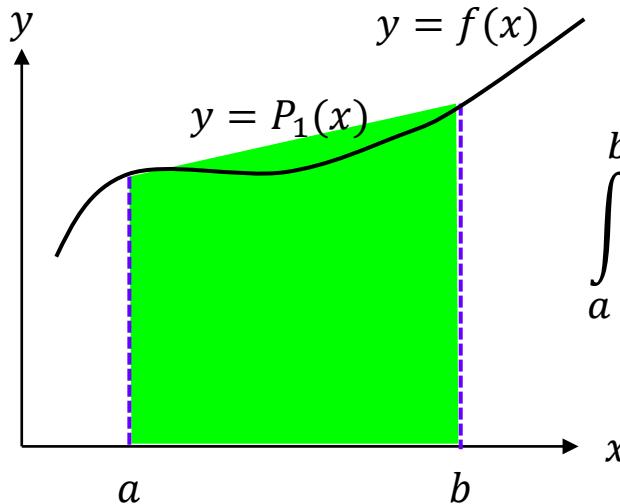
*Third-Order-Accurate*

**Simpson's Rule**

$$\phi^T = - \sum_{j \in T} \frac{\vec{\lambda} \cdot \vec{n}_j}{6} [u_m + 4 u_{mid,j} + u_p]$$

## Trapezoidal Rule

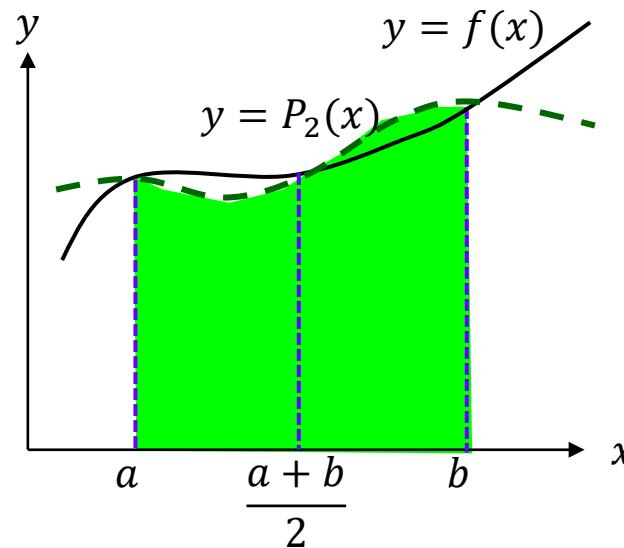
If  $f \in C^2[a, b]$ , then a number  $\xi$  in  $[a, b]$  exists with



$$\int_a^b f(x) dx = \frac{f(a) + f(b)}{2} (b - a) - \frac{f''(\xi)}{12} (b - a)^3$$

## Simpson's Rule

If  $f \in C^4[a, b]$ , then a number  $\xi$  in  $[a, b]$  exists and



$$\int_a^b f(x) dx = \frac{(b - a)}{6} \left[ f(a) + 4 f\left(\frac{a + b}{2}\right) + f(b) \right] - \frac{f^{(4)}(\xi)}{2880} (b - a)^5$$

# Aux Residual using Trapezoidal Rule

$$\phi^T = + \sum_{j \in T} k_j u_j$$

$$\vec{F}(u) = u \vec{\lambda}$$

$$\iint_S \nabla \cdot \vec{F} dx dy = \oint_{\partial S} \vec{F} \cdot \hat{n}_{ext} dl$$

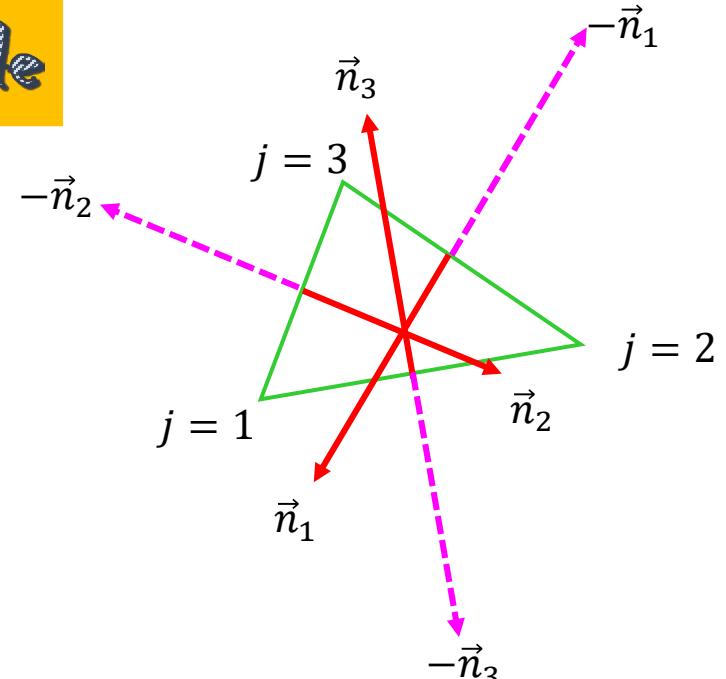
$$= \frac{u_2 \vec{\lambda} + u_1 \vec{\lambda}}{2} \cdot (-\vec{n}_3) + \frac{u_3 \vec{\lambda} + u_2 \vec{\lambda}}{2} \cdot (-\vec{n}_1) + \frac{u_1 \vec{\lambda} + u_3 \vec{\lambda}}{2} \cdot (-\vec{n}_2)$$

$$= \frac{u_1 \vec{\lambda}}{2} \cdot (-\vec{n}_2 - \vec{n}_3) + \frac{u_2 \vec{\lambda}}{2} \cdot (-\vec{n}_1 - \vec{n}_3) + \frac{u_3 \vec{\lambda}}{2} \cdot (-\vec{n}_1 - \vec{n}_2)$$

$$= \frac{u_1 \vec{\lambda}}{2} \cdot \vec{n}_1 + \frac{u_2 \vec{\lambda}}{2} \cdot \vec{n}_2 + \frac{u_3 \vec{\lambda}}{2} \cdot \vec{n}_3$$

$$= k_1 u_1 + k_2 u_2 + k_3 u_3$$

where  $k_j = \frac{\vec{\lambda} \cdot \vec{n}_j}{2}$



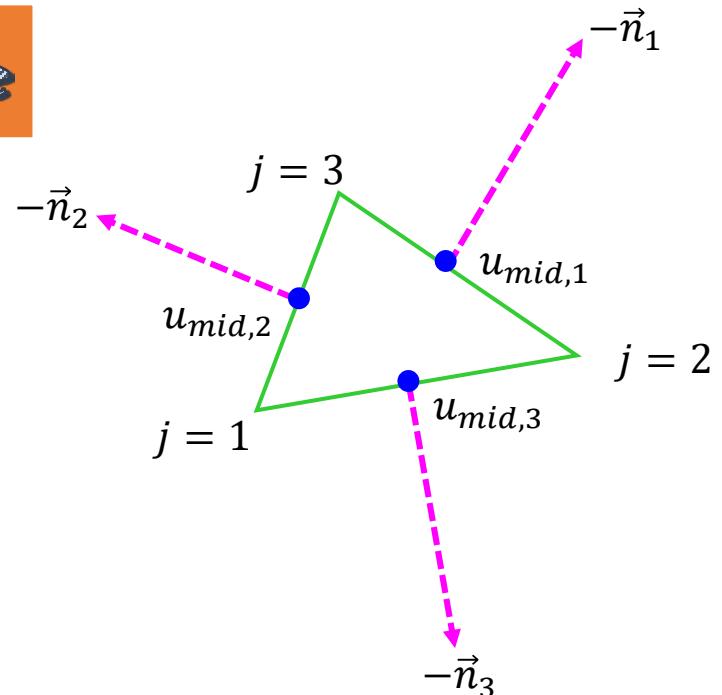
# Flux Residual using Simpson's Rule

$$\phi^T = - \sum_{j \in T} \frac{\vec{\lambda} \cdot \vec{n}_j}{6} [u_m + 4 u_{mid,j} + u_p]$$

$$\vec{F}(u) = u \vec{\lambda}$$

$$\iint_S \nabla \cdot \vec{F} dx dy = \oint_{\partial S} \vec{F} \cdot \hat{n}_{ext} dl$$

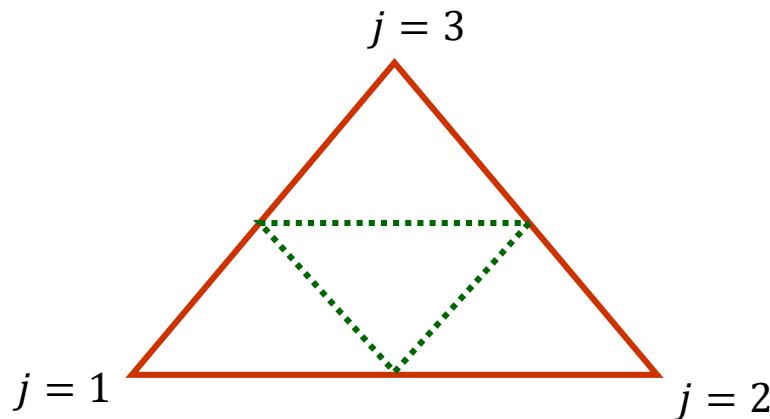
$$= \frac{1}{6} [u_1 \vec{\lambda} + 4 u_{mid,3} + u_2 \vec{\lambda}] \cdot (-\vec{n}_3) + \frac{1}{6} [u_2 \vec{\lambda} + 4 u_{mid,1} + u_3 \vec{\lambda}] \cdot (-\vec{n}_1) \\ + \frac{1}{6} [u_1 \vec{\lambda} + 4 u_{mid,1} + u_3 \vec{\lambda}] \cdot (-\vec{n}_2)$$



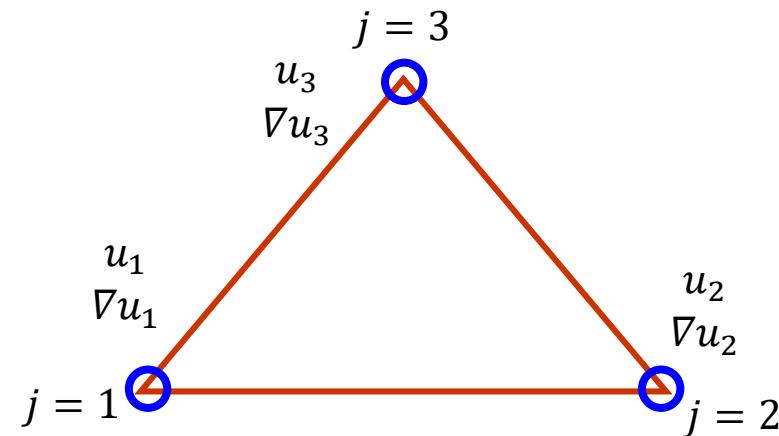
# Third-Order-Accurate : Steady

To find the  $u_{mid,j}$  is always a concern. There are two ways of doing it:

- 1) Submesh Reconstruction
- 2) Gradient Recovery



*Submesh Reconstruction*

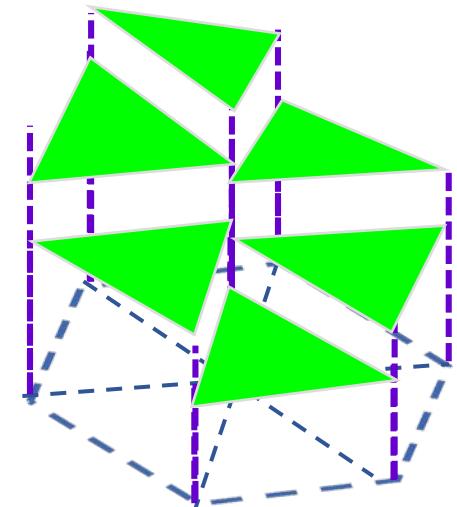


*Gradient Recovery*

## Gradient Recovery

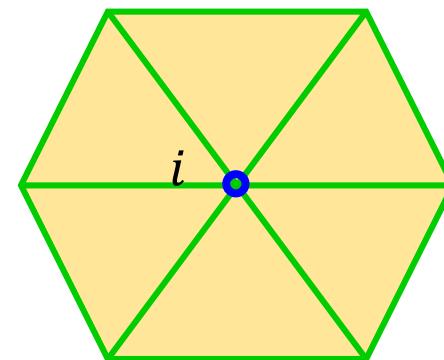
**Step 1 :** Find the gradient for each cell using Green-Gauss theorem. The gradient for each cell is always a constant

$$\nabla u^T = \frac{1}{S_T} \oint_{\partial T} u \vec{n} \cdot d\Gamma = \frac{1}{2S_T} \sum_{j \in T} u \vec{n}_j$$



**Step 2 :** The nodal gradient at node  $i$  is taken as the weighted average of  $\nabla u^T$  from the cell sharing it.

$$\nabla u_i = \frac{\sum_{T \in \cup \Delta_i} S_T \nabla u^T}{\sum_{T \in \cup \Delta_i} S_T}$$



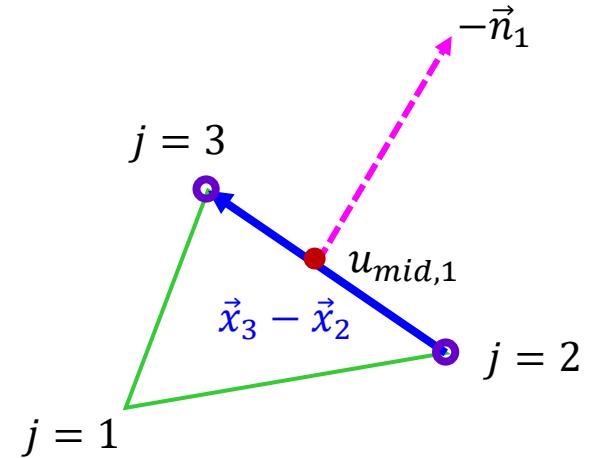
Similar procedures are applied until all the nodal gradient has been evaluated.

**Step 3** : Estimating the value of  $u_{mid,j}$ . Take note that the position of the mid-point,  $\vec{x}_m$  is never sought.

$$u_{mid,j} = \frac{u_m + u_p}{2} + \frac{\nabla u_m - \nabla u_p}{8} \cdot (\vec{x}_p - \vec{x}_m)$$

For example,  $u_{mid,1}$  is sought as letting

$$m = 2 \quad p = 3$$



**Step 4** : Finally, evaluate the flux residual of a cell using Simpson's rule.

$$\phi^T = - \sum_{j \in T} \frac{\vec{\lambda} \cdot \vec{n}_j}{6} [u_m + 4 u_{mid,j} + u_p]$$

# Third-Order-Accurate : Unsteady

Aside to the two conditions mentioned for steady case, for unsteady problem, the time derivative has to be third-order-accurate in **time** (i.e.  $\Delta t^3$ ) to give the scheme third-order-accurate in **both time and space**.

$$\sum_{T \in \cup \Delta_i} \left\{ \sum_{j \in T} m_{ij}^T \frac{\partial u_j(t)}{\partial t} + \underbrace{\beta_i^T \phi^T}_{\text{Steady residual / flux residual}} \right\} = 0 + O(h^4)$$

*Unsteady residual*

For the sake of brevity, let us re-write the unsteady residual as

$$\sum_{T \in \cup \Delta_i} \{ \psi_i^T + \phi_i^T \} \cong 0$$

The evaluation of flux residual is already mentioned in previous slides.

The unsteady residual is evaluated as following:

$$\psi_i^T = \left( \beta_j^T - \frac{1}{3} \right) \sum_{j \in T} \frac{S_T}{3} \left( \frac{\partial u}{\partial t} \right)_j + \frac{1}{3} \sum_{j \in T} \frac{S_T}{3} \left( \frac{\partial u}{\partial t} \right)_{mid,j}$$

where

$$\left( \frac{\partial u}{\partial t} \right)_j = \frac{11 u_j^{n+1} - 18 u_j^n + 9 u_j^{n-1} - 2 u_j^{n-2}}{6 \Delta t} + O(\Delta t^3)$$

$$\left( \frac{\partial u}{\partial t} \right)_{mid,j} = \frac{11 u_{mid,j}^{n+1} - 18 u_{mid,j}^n + 9 u_{mid,j}^{n-1} - 2 u_{mid,j}^{n-2}}{6 \Delta t} + O(\Delta t^3)$$

Finally, the equation of system at time level  **$n + 1$**  is approximated using dual-time-stepping

$$u_i^{n+1,k+1} = u_i^{n+1,k} - \frac{\Delta \tau}{S_i} \sum_{T \in \cup \Delta_i} (\psi_i^T + \phi_i^T)^{n+1,k}$$

# Numerical Results

Steady Case : Linear & Circular Advection

Unsteady Case : Linear & Circular Advection

# Steady Case : Linear Advection

Constant linear advection speed :

$$\vec{\lambda} = (2,1)^T$$

Domain :

$$\Omega = [0,1]^2 \subseteq \mathbb{R}^2$$

Initial Guess :

$$u(x, y) = \begin{cases} \cos(\pi x) & ; \quad y = 0 \\ 0 & ; \quad 0 < y \leq 1 \end{cases}$$

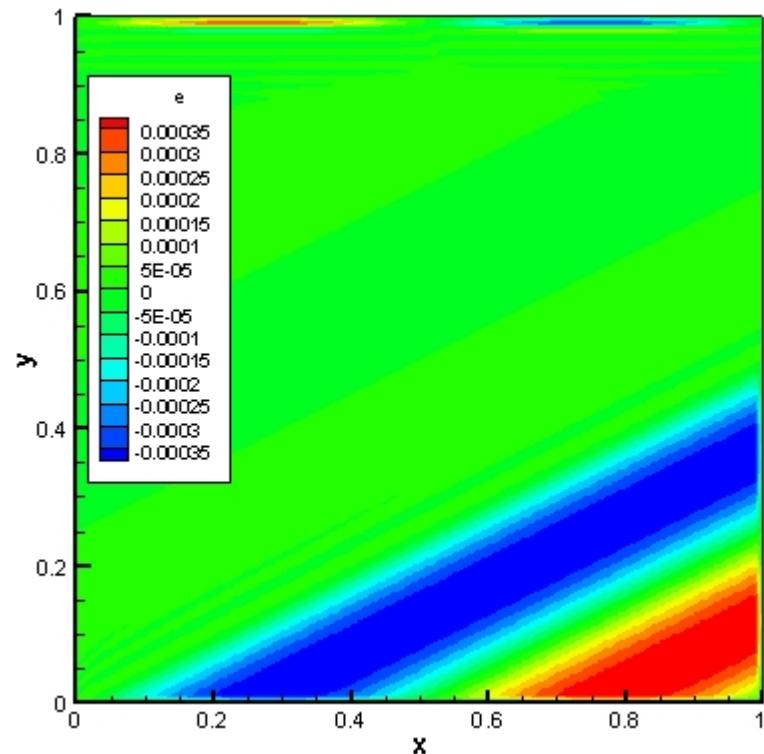
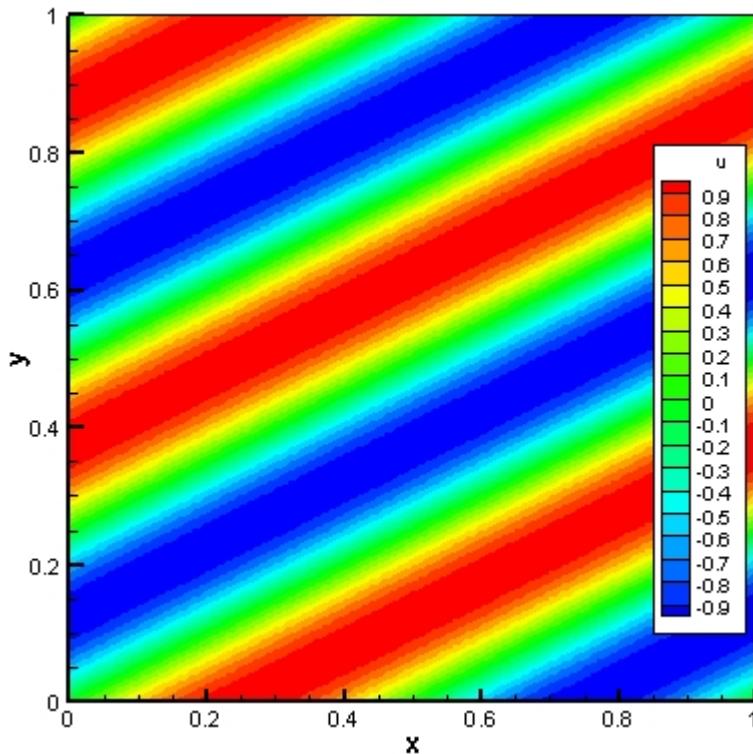
Exact solution (for steady state) :

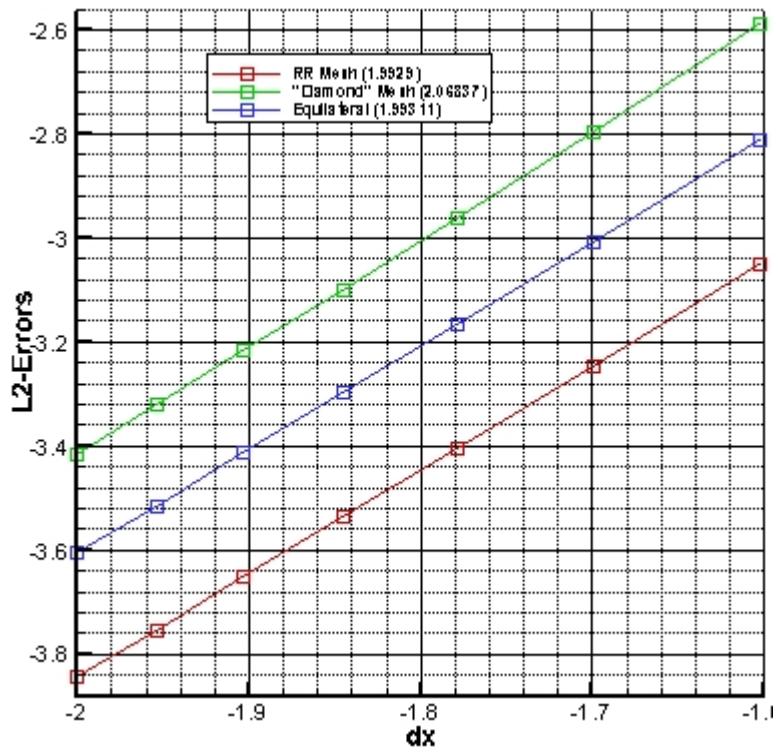
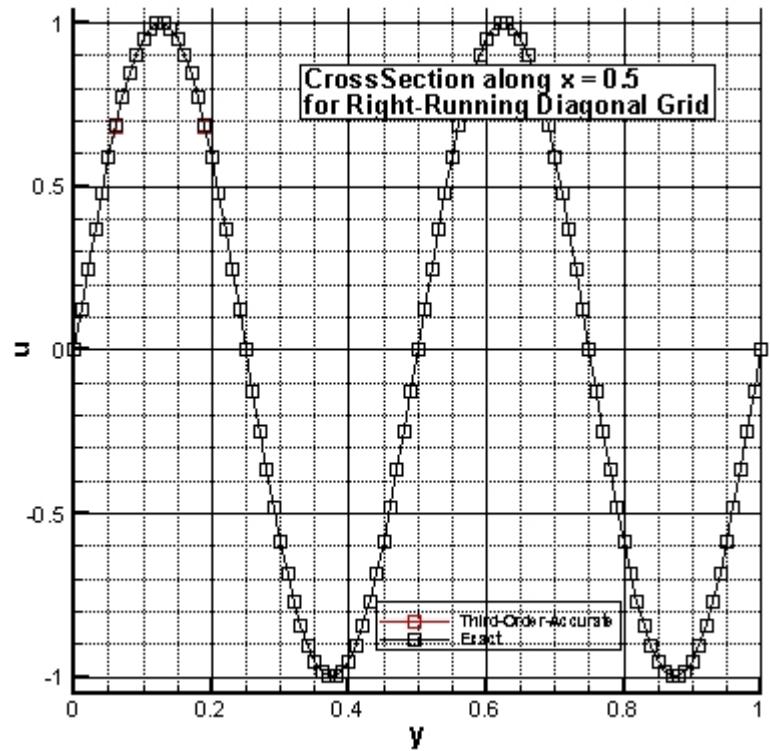
$$u(x, y) = \cos[\pi(x - 2y)]$$

Boundary Conditions :

The boundaries are always set to the exact solution.

$$u(x, y) = \cos[\pi(x - 2y)] \quad \text{for} \quad (x, y) \in \partial\Omega$$





# Steady Case : Circular Advection

Averaged circular velocity :

$$\tilde{\lambda} = (\tilde{y}, -\tilde{x})^T \quad \text{where} \quad \tilde{x} = \frac{1}{3} \sum_{j \in T} x_j \quad \tilde{y} = \frac{1}{3} \sum_{j \in T} y_j$$

Domain :

$$\Omega = [-1,1] \times [0,1] \subseteq \mathbb{R}^2$$

Initial Guess :

$$u(x, y) = \begin{cases} G(x) & , \{(x, y): -0.75 \leq x \leq -0.25, y = 0\} \\ G(-x) & , \{(x, y): 0.25 \leq x \leq 0.75, y = 0\} \\ 0 & otherwise \end{cases}$$

in which  $G(x) = \begin{cases} g(4x + 3) & , \{(x, y): -0.75 \leq x \leq -0.5, y = 0\} \\ g(-4x - 1) & , \{(x, y): -0.5 \leq x \leq -0.25, y = 0\} \end{cases}$

where  $g(x) = x^5(70x^4 - 315x^3 + 540x^2 - 420x + 126)$

Boundary Conditions :

$$u(x, y) = \begin{cases} G(x) & \{(x, y): -0.75 \leq x \leq -0.25, y = 0\} \\ G(-x) & \{(x, y): 0.25 \leq x \leq 0.75, y = 0\} \\ 0 & (A \cup B \cup C) \cup \{(x, y): x = -1\} \cup \{(x, y): x = 1\} \cup \{(x, y): y = 1\} \end{cases}$$

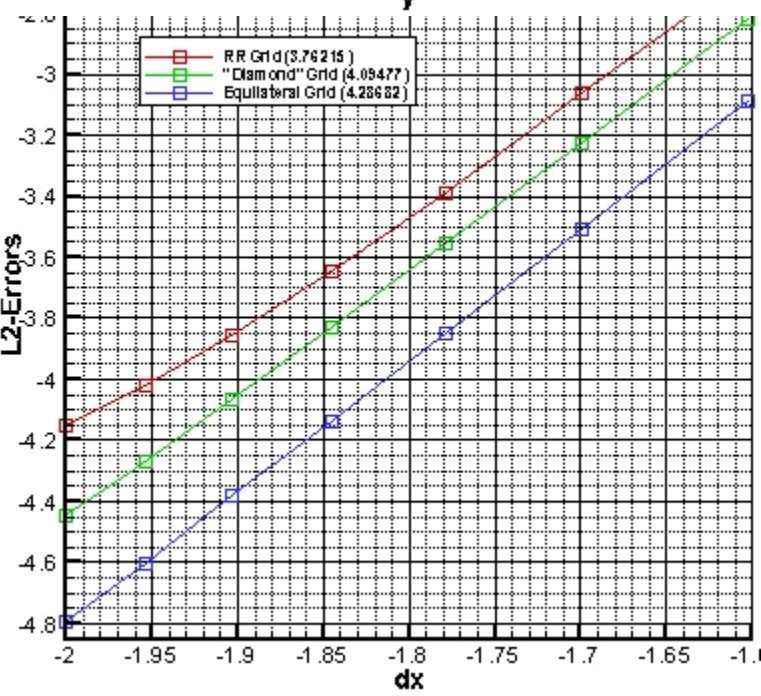
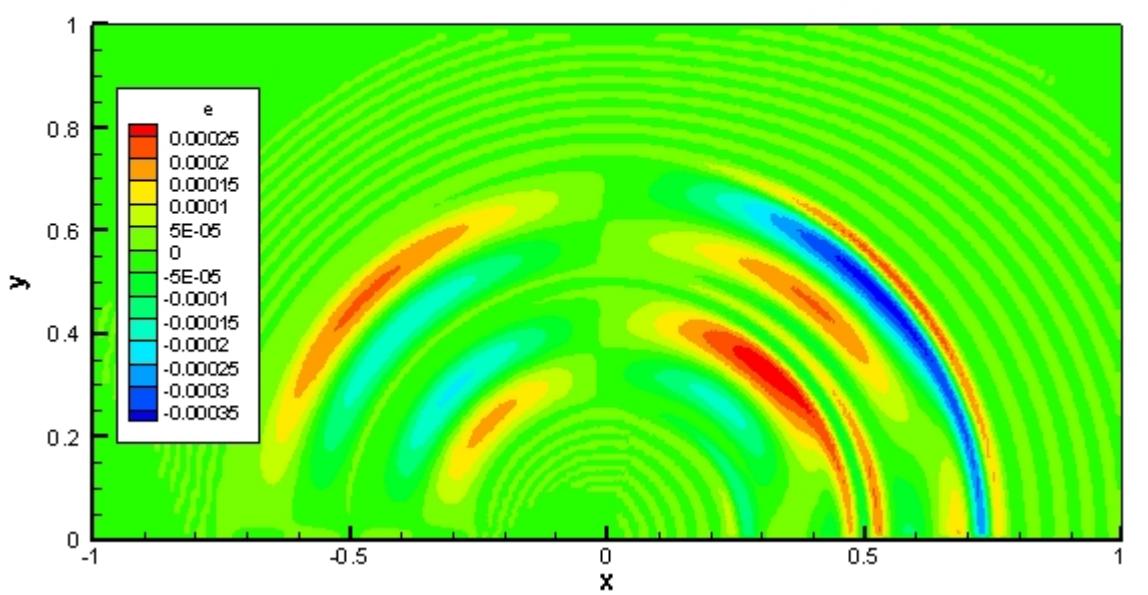
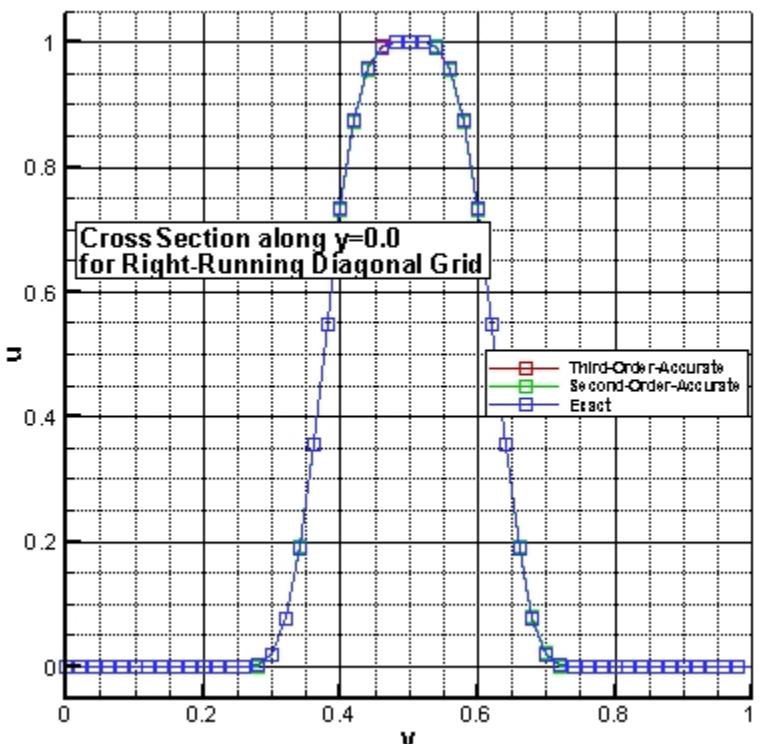
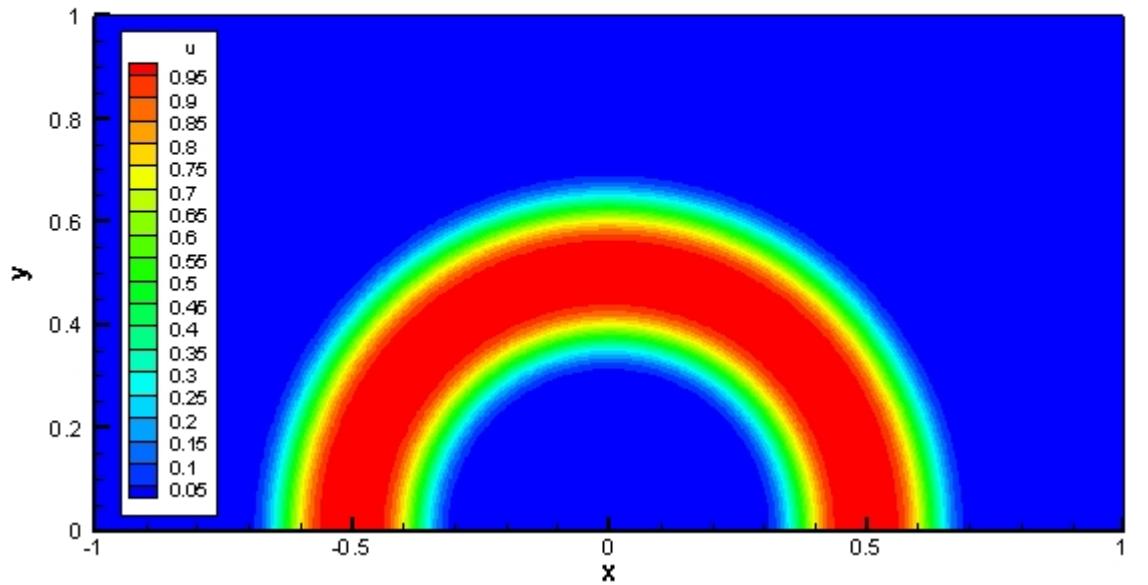
where  $A = \{(x, y): -1 \leq x \leq -0.75, y = 0\}$

$B = \{(x, y): -0.25 \leq x \leq 0.25, y = 0\}$

$C = \{(x, y): 0.75 \leq x \leq 1, y = 0\}$

Exact solution (for steady state) :

$$u(x, y) = \begin{cases} G(-r) & , \quad 0.25 \leq r \leq 0.75 \\ 0 & , \quad elsewhere \end{cases} \quad \text{where} \quad r = \sqrt{x^2 + y^2}$$



# Unsteady Case : Linear Advection

Constant linear advection speed :

$$\vec{\lambda} = (1, 2)^T$$

Domain :

$$\Omega_t = \Omega \times [0, t_f] = [0, 1]^2 \times [0, 1] \subseteq \mathbb{R}^2 \times \mathbb{R}^+$$

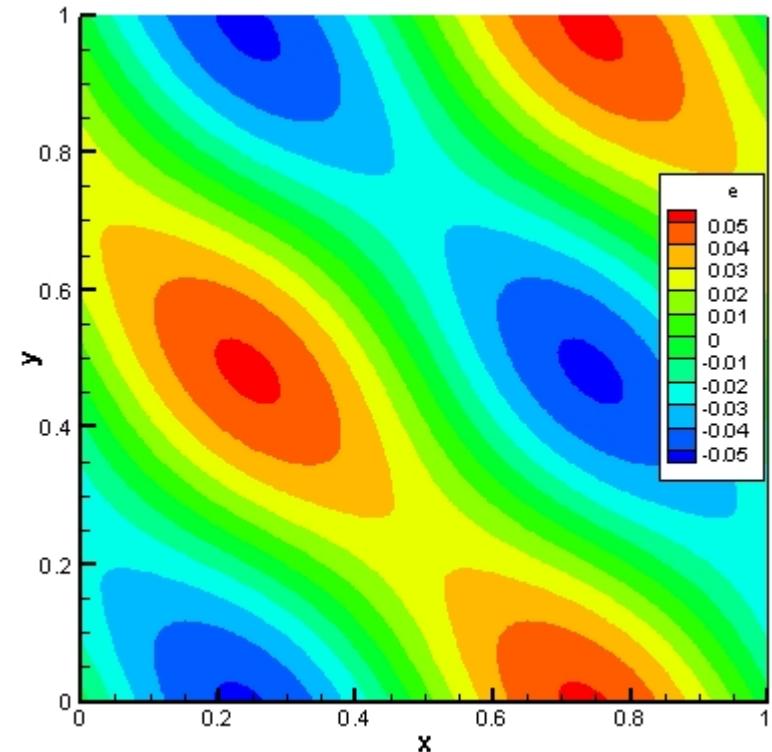
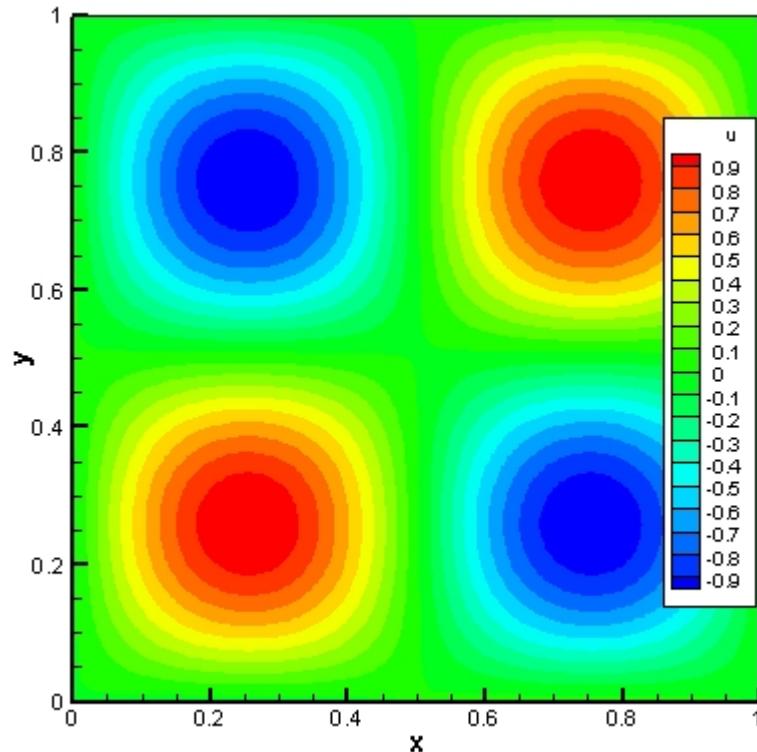
Initial Condition :

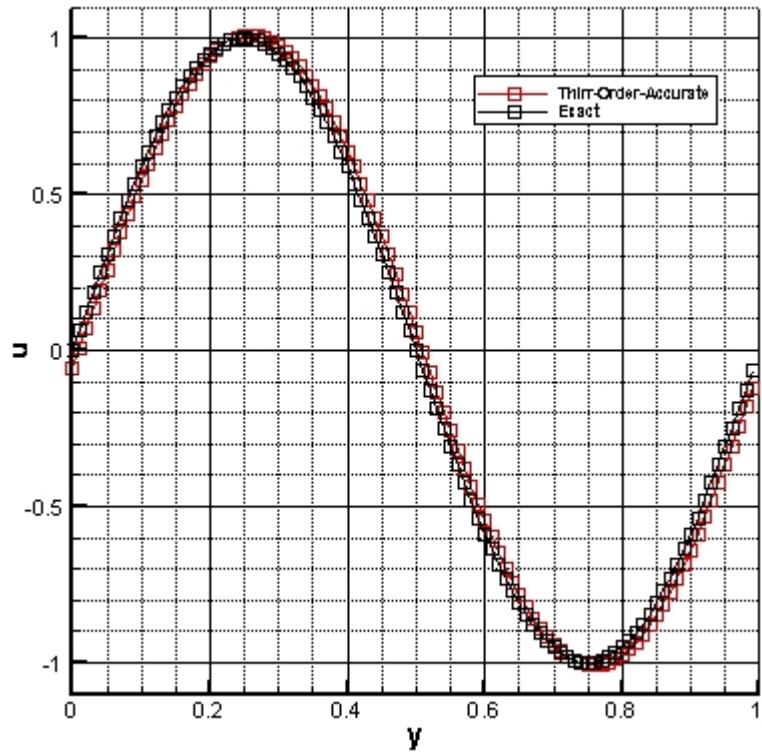
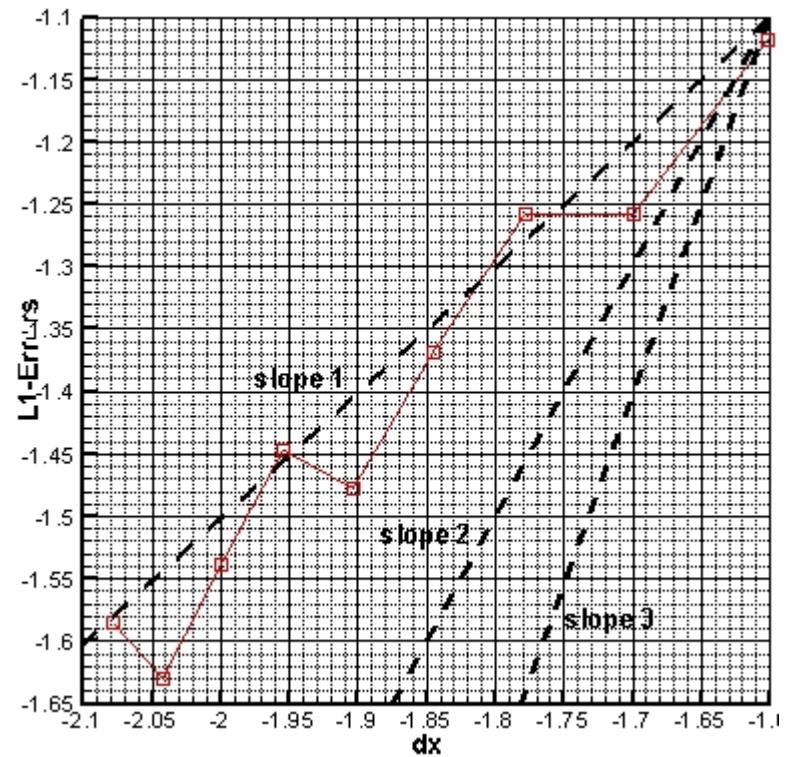
$$u(x, y, 0) = u(x, y, 1) = \sin(2\pi x) \sin(2\pi y)$$

Final solution :

Boundary Conditions :

Periodic boundary condition for  $(x, y) \in \partial\Omega$





# Unsteady Case : Circular Advection

Averaged circular velocity :

$$\tilde{\vec{\lambda}} = (-2\pi\tilde{y}, 2\pi\tilde{x})^T \quad \text{where}$$

$$\tilde{x} = \frac{1}{3} \sum_{j \in T} x_j$$

$$\tilde{y} = \frac{1}{3} \sum_{j \in T} y_j$$

Domain :

$$\Omega_t = \Omega \times [0, t_f] = [1, 1]^2 \times [0, 1] \subseteq \mathbb{R}^2 \times \mathbb{R}^+$$

Initial Condition :

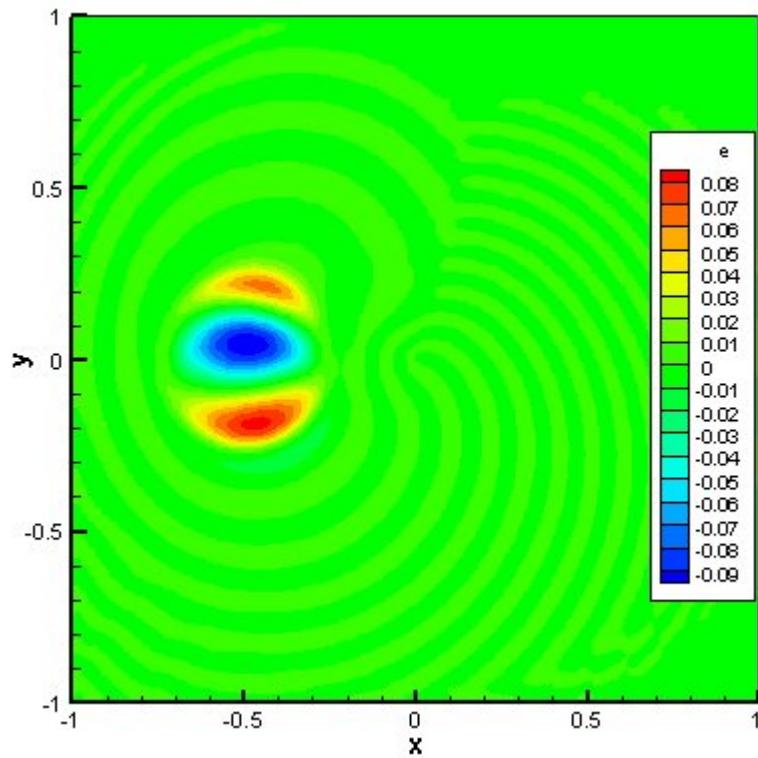
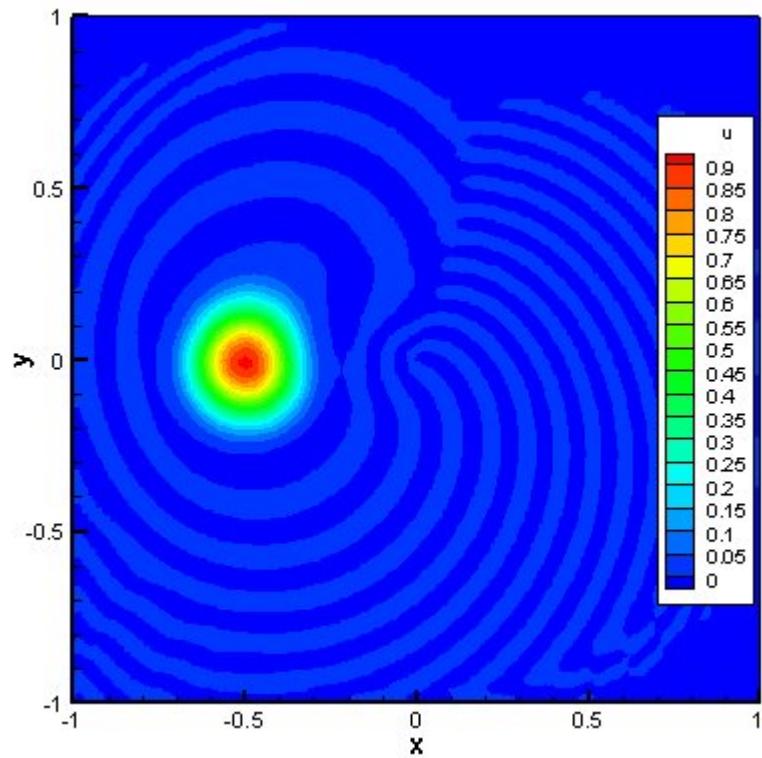
$$u(x, y, 0) = u(x, y, 1) = \begin{cases} \cos^2(2\pi r) & r \leq 0.25 \\ 0 & r > 0.25 \end{cases} \quad \text{where} \quad r = \sqrt{(x + 0.5)^2 + y^2}$$

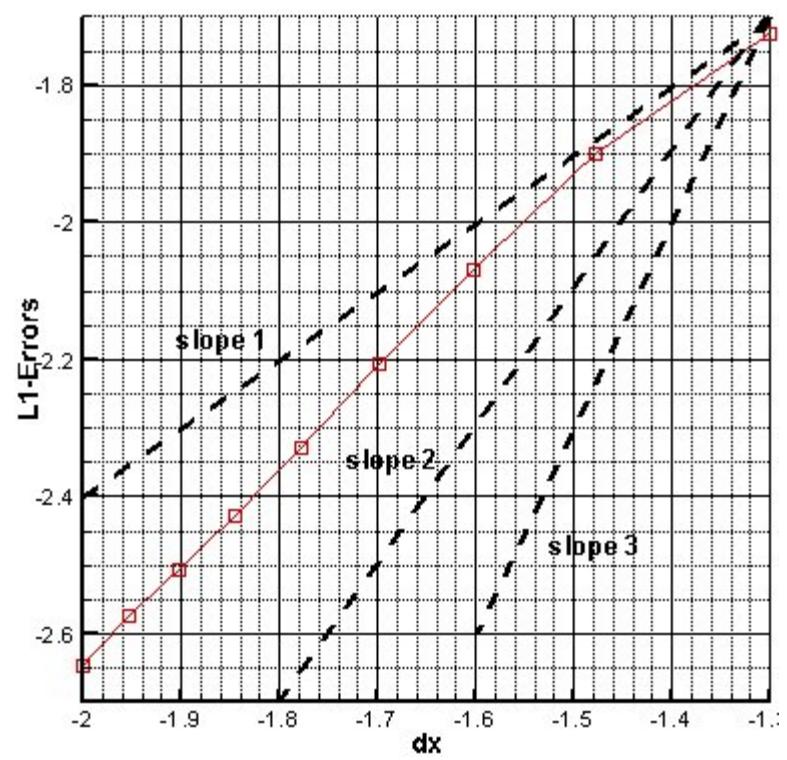
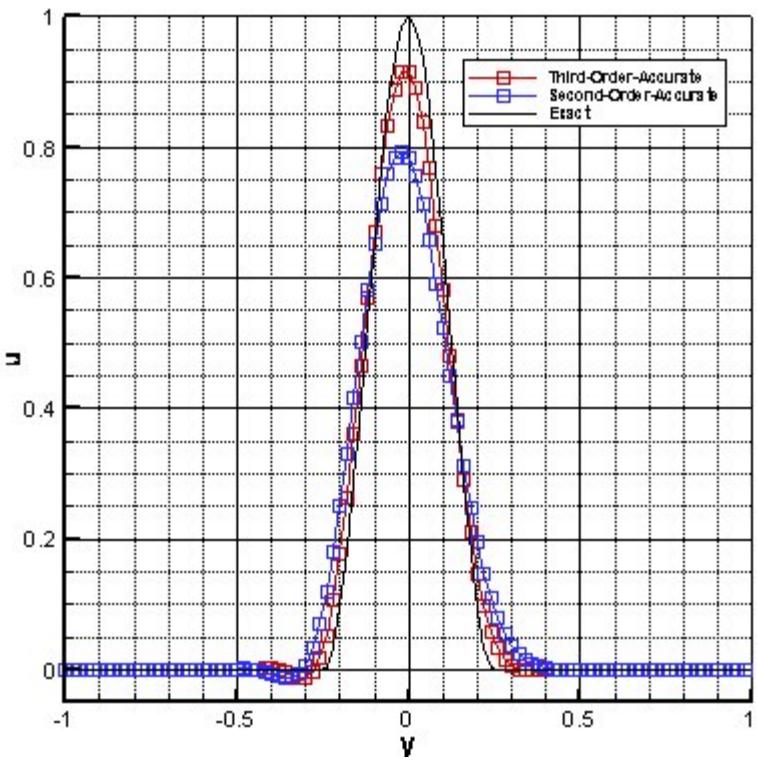
Final solution :

Boundary Conditions :

All the boundaries are always set to be 0.

$$u(x, y, t) = 0 \quad \text{for} \quad (x, y) \in \partial\Omega$$





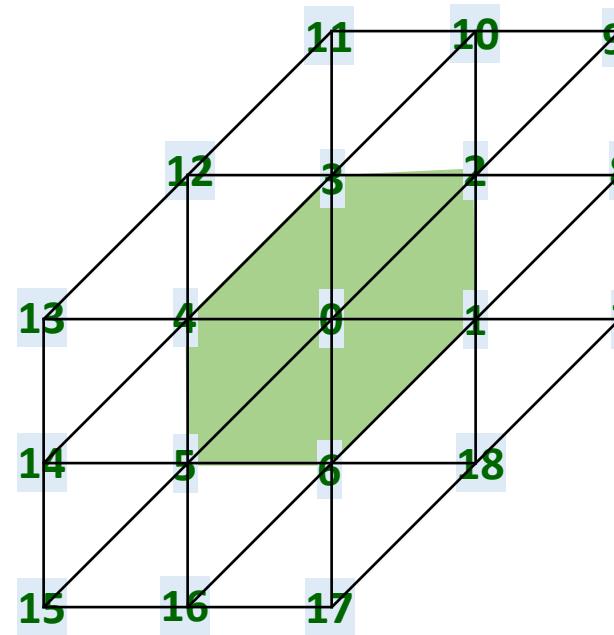
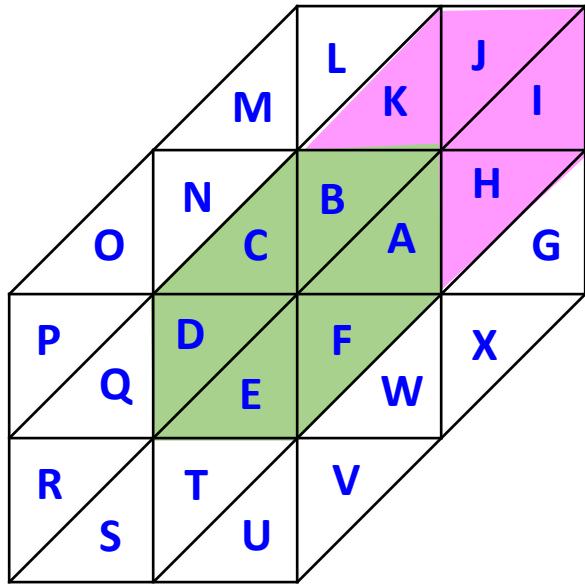
# Truncation Errors Analysis

Steady Case :  $a_x > a_y$

Unsteady Case :  $a_x < a_y$

# Truncation Errors : Steady

The disadvantage of using gradient recovery approach in estimating  $u_{mid,j}$  is that the scheme is no longer on compact stencil.



Expand the Taylor's expansion series in  $x$  and  $y$ -coordinates. For examples,

$$u_1 = u_0 + \Delta x \frac{\partial u_0}{\partial x} + \frac{1}{2} \Delta x^2 \frac{\partial^2 u_0}{\partial x^2} + O(\Delta x^3)$$

$$u_8 = u_0 + \left( (2 \Delta x) \frac{\partial u_0}{\partial x} + (\Delta y) \frac{\partial u_0}{\partial y} \right) + \left( (2 \Delta x)^2 \frac{\partial^2 u_0}{\partial x^2} + 2 (2 \Delta x)(\Delta y) \frac{\partial^2 u_0}{\partial x \partial y} + (\Delta y)^2 \frac{\partial^2 u_0}{\partial y^2} \right) + O(\Delta x^3, \Delta y^3)$$

$$u_{16} = u_0 + \left( (-\Delta x) \frac{\partial u_0}{\partial x} + (-2 \Delta y) \frac{\partial u_0}{\partial y} \right) + \left( (-\Delta x)^2 \frac{\partial^2 u_0}{\partial x^2} + 2 (-\Delta x)(-2 \Delta y) \frac{\partial^2 u_0}{\partial x \partial y} + (-2 \Delta y)^2 \frac{\partial^2 u_0}{\partial y^2} \right) + O(\Delta x^3, \Delta y^3)$$

**Step 1** : Evaluate cell gradient using the formula:

$$\nabla u^T = \frac{1}{2S_T} \sum_{j \in T} u \vec{n}_j$$

For examples,

$$\nabla u^A = \left( \frac{u_1 - u_0}{\Delta x} \right) \hat{i} + \left( \frac{u_2 - u_1}{\Delta y} \right) \hat{j} \quad \nabla u^J = \left( \frac{u_9 - u_{10}}{\Delta x} \right) \hat{i} + \left( \frac{u_{10} - u_2}{\Delta y} \right) \hat{j}$$

**Step 2** : Find the nodal gradient numerically, using the results from step 1.

$$\nabla u_i = \frac{\sum_{T \in \cup \Delta_i} S_T \nabla u^T}{\sum_{T \in \cup \Delta_i} S_T}$$

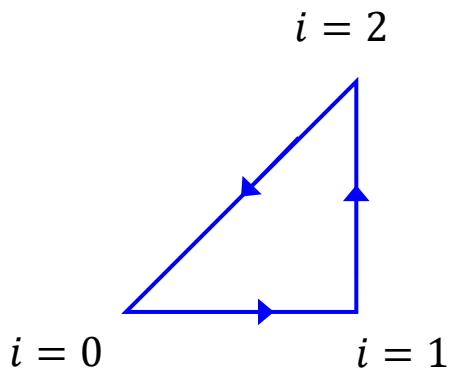
For example,

$$\nabla u_0 = \left( \frac{2u_1 + u_2 - u_3 - 2u_4 - u_5 + u_6}{\Delta x} \right) \hat{i} + \left( \frac{u_2 - u_1 + 2u_3 + u_4 - u_5 - 2u_6}{\Delta y} \right) \hat{j}$$

**Step 3** : Evaluate the flux residual using Simpson's rule.

$$\phi^T = - \sum_{j \in T} \frac{\vec{\lambda} \cdot \vec{n}_j}{6} [u_m + 4 u_{mid,j} + u_p] = - \sum_{j \in T} \frac{k_j}{3} [u_m + 4 u_{mid,j} + u_p]$$

For triangular cell  $T = A$



$$\begin{aligned}\phi^A &= -\frac{k_0^A}{3} \left[ 3 u_1 + 3 u_2 - \frac{1}{2} \Delta y \hat{j} \cdot (\nabla u_2 - \nabla u_1) \right] \\ &\quad - \frac{k_1^A}{3} \left[ 3 u_0 + 3 u_2 + \frac{1}{2} \Delta x \hat{i} \cdot (\nabla u_0 - \nabla u_2) + \frac{1}{2} \Delta y \hat{j} \cdot (\nabla u_0 - \nabla u_2) \right] \\ &\quad - \frac{k_2^A}{3} \left[ 3 u_0 + 3 u_1 - \frac{1}{2} \Delta x \hat{i} \cdot (\nabla u_1 - \nabla u_0) \right]\end{aligned}$$

where

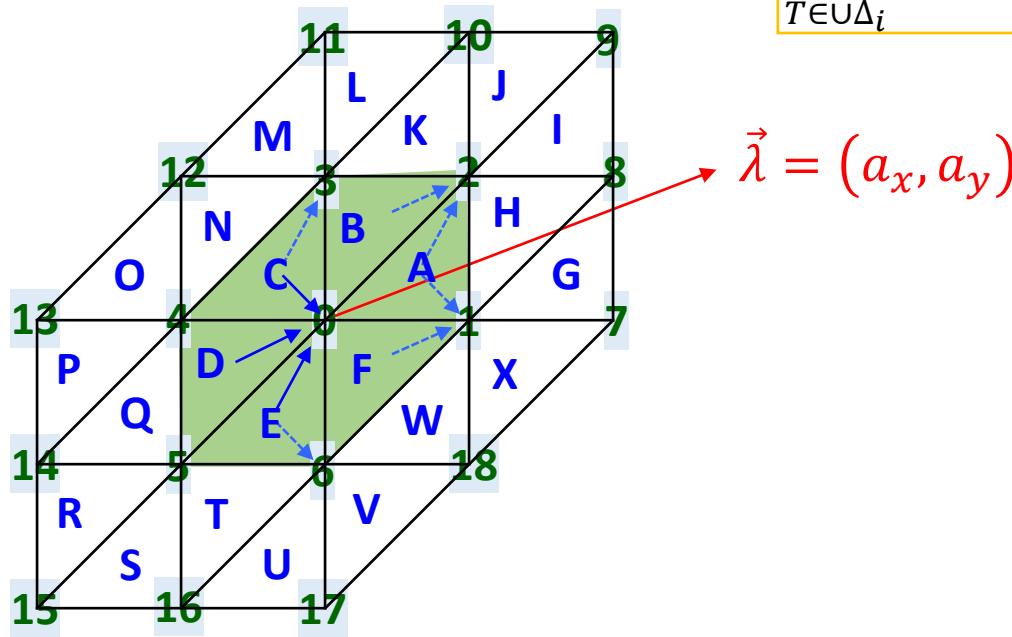
$$k_0^A = -\frac{1}{2} a_x \Delta y$$

$$k_1^A = \frac{1}{2} a_x \Delta y - \frac{1}{2} a_y \Delta x$$

$$k_2^A = \frac{1}{2} a_y \Delta x$$

Step 4 : Assembling the flux residual to node  $i = 0$ .

$$\sum_{T \in \cup \Delta_i} \{\beta_i^T \phi^T\} \cong 0$$



For linear advection speed  $a_x > a_y$ , as illustrated in figure above, only element  $T = C, D, E$  will contribute to node  $i = 0$ .

$$\sum_{T \in \cup \Delta_0} \beta_0^T \phi^T = \beta_0^C \phi^C + \beta_0^D \phi^D + \beta_0^E \phi^E$$

From  $T = C$

$$\beta_0^C = 1 - \frac{a_y \Delta x}{a_x \Delta y}$$

$$\begin{aligned}\phi^C &= -\frac{k_0^C}{3} \left[ 3\textcolor{red}{u}_0 + 3\textcolor{red}{u}_3 - \frac{1}{2} \Delta y \hat{j} \cdot (\nabla u_3 - \nabla u_0) \right] \\ &\quad - \frac{k_1^C}{3} \left[ 3\textcolor{red}{u}_3 + 3\textcolor{red}{u}_4 + \left( \frac{1}{2} \Delta x \hat{i} + \frac{1}{2} \Delta y \hat{j} \right) \cdot (\nabla u_4 - \nabla u_3) \right] \\ &\quad - \frac{k_2^C}{3} \left[ 3\textcolor{red}{u}_0 + 3\textcolor{red}{u}_4 - \frac{1}{2} \Delta x \hat{i} \cdot (\nabla u_0 - \nabla u_4) \right]\end{aligned}$$

where  $k_0^C = -\frac{1}{2} a_x \Delta y$

$$k_1^C = \frac{1}{2} a_x \Delta y - \frac{1}{2} a_y \Delta x \quad k_2^C = \frac{1}{2} a_y \Delta x$$

From  $T = D$

$$\beta_0^D = 1$$

$$\begin{aligned}\phi^D &= -\frac{k_5^D}{3} \left[ 3\textcolor{red}{u}_0 + 3\textcolor{red}{u}_4 + \frac{1}{2} \Delta x \hat{i} \cdot (\nabla u_4 - \nabla u_0) \right] \\ &\quad - \frac{k_0^D}{3} \left[ 3\textcolor{red}{u}_4 + 3\textcolor{red}{u}_5 + \frac{1}{2} \Delta y \hat{j} \cdot (\nabla u_5 - \nabla u_4) \right] \\ &\quad - \frac{k_4^D}{3} \left[ 3\textcolor{red}{u}_0 + 3\textcolor{red}{u}_5 - \left( \frac{1}{2} \Delta x \hat{i} + \frac{1}{2} \Delta y \hat{j} \right) \hat{i} \cdot (\nabla u_0 - \nabla u_5) \right]\end{aligned}$$

where  $k_5^D = -\frac{1}{2} a_y \Delta x$

$$k_0^D = \frac{1}{2} a_x \Delta y \quad k_4^D = -\frac{1}{2} a_x \Delta y + \frac{1}{2} a_y \Delta x$$

From  $T = E$

$$\beta_0^E = \frac{a_y \Delta x}{a_x \Delta y}$$

$$\begin{aligned}\phi^E &= -\frac{k_5^E}{3} \left[ 3\textcolor{red}{u}_0 + 3\textcolor{red}{u}_6 - \frac{1}{2} \Delta y \hat{j} \cdot (\nabla u_0 - \nabla u_6) \right] \\ &\quad - \frac{k_6^E}{3} \left[ 3\textcolor{red}{u}_0 + 3\textcolor{red}{u}_5 + \left( \frac{1}{2} \Delta x \hat{i} + \frac{1}{2} \Delta y \hat{j} \right) \cdot (\nabla u_5 - \nabla u_0) \right] \\ &\quad - \frac{k_0^E}{3} \left[ 3\textcolor{red}{u}_5 + 3\textcolor{red}{u}_6 - \frac{1}{2} \Delta x \hat{i} \cdot (\nabla u_5 - \nabla u_6) \right]\end{aligned}$$

where  $k_5^E = -\frac{1}{2} a_x \Delta y$

$$k_6^E = \frac{1}{2} a_x \Delta y - \frac{1}{2} a_y \Delta x \quad k_0^E = \frac{1}{2} a_y \Delta x$$

# Truncation Errors : Unsteady

The flux residual at time level  $n + 1$  is evaluated exactly the same as for the steady case.

However, when it comes to the unsteady residual, time has to be considered as the third variable.

$$\begin{aligned} & u(t^{n+1} \pm \Delta t, x_0 \pm \Delta x, y_0 \pm \Delta y) \\ &= u_0^{n+1} + \left( (\pm \Delta t) \frac{\partial}{\partial t} + (\pm \Delta x) \frac{\partial}{\partial x} + (\pm \Delta y) \frac{\partial}{\partial y} \right) u_0^{n+1} \\ &+ \frac{1}{2} \left( (\pm \Delta t)^2 \frac{\partial^2}{\partial t^2} + (\pm \Delta x)^2 \frac{\partial^2}{\partial x^2} + (\pm \Delta y)^2 \frac{\partial^2}{\partial y^2} + 2(\pm \Delta t)(\pm \Delta x) \frac{\partial^2}{\partial t \partial x} + 2(\pm \Delta t)(\pm \Delta y) \frac{\partial^2}{\partial t \partial y} \right. \end{aligned}$$

Steps employed in approximating  $u_{mid,j}$  have to be repeated here, but with the Taylor's expansion series including the time,  $u(t^{n+1} \pm \Delta t, x_0 \pm \Delta x, y_0 \pm \Delta y)$

The contribution of unsteady residual from each element to node  $i = 0$  has to be considered.

$$\sum_{T \in \cup \Delta_i} \{\psi_i^T + \phi_i^T\} \approx 0$$

where the unsteady residual generally involves discretization of time derivative to third-order-accurate in time.

$$\left( \frac{\partial u}{\partial t} \right)_j = \frac{11 u_j^{n+1} - 18 u_j^n + 9 u_j^{n-1} - 2 u_j^{n-2}}{6 \Delta t} + O(\Delta t^3)$$

$$\left( \frac{\partial u}{\partial t} \right)_{mid,j} = \frac{11 u_{mid,j}^{n+1} - 18 u_{mid,j}^n + 9 u_{mid,j}^{n-1} - 2 u_{mid,j}^{n-2}}{6 \Delta t} + O(\Delta t^3)$$

## TE analysis for Steady Case

linear advection speed  $a_x > a_y$

$$\sum_{T \in \cup \Delta_i} (\beta_i^T \phi_i^T) = \Delta x \Delta y \left( a_x \frac{\partial}{\partial x} + a_y \frac{\partial}{\partial y} \right) u_0 - \frac{1}{2} \frac{\Delta x^2 \Delta y}{a_x} \left( a_x^2 \frac{\partial^2}{\partial x^2} + a_y^2 \frac{\partial^2}{\partial y^2} + 2a_x a_y \frac{\partial^2}{\partial x \partial y} \right) u_0 + O(\Delta x^3, \Delta y^3) \quad \text{--(a)}$$

From the governing equation,

$$a_x \frac{\partial u}{\partial x} + a_y \frac{\partial u}{\partial y} = 0 \quad \text{--(b)}$$

Multiply by  $a_x$  and differentiate w.r.t  $x$

$$a_x \frac{\partial}{\partial x} \left( a_x \frac{\partial u}{\partial x} + a_y \frac{\partial u}{\partial y} \right) = a_x \frac{\partial}{\partial x} (0)$$

Multiply by  $a_y$  and differentiate w.r.t  $y$



$$a_y \frac{\partial}{\partial y} \left( a_x \frac{\partial u}{\partial x} + a_y \frac{\partial u}{\partial y} \right) = a_y \frac{\partial}{\partial y} (0)$$

$$a_x^2 \frac{\partial^2 u}{\partial x^2} + 2 a_x a_y \frac{\partial^2 u}{\partial x \partial y} + a_y^2 \frac{\partial^2 u}{\partial y^2} = 0 \quad \text{--(c)}$$

Substitute equations (b) and (c) into (a),

$$\sum_{T \in \cup \Delta_i} (\beta_i^T \phi_i^T) = O(\Delta x^3, \Delta y^3)$$

## TE analysis for Unsteady Case

linear advection speed  $a_x < a_y$

$$\sum_{T \in \Delta_i} (\psi_i^T + \phi_i^T)^{n+1} = \Delta x \Delta y \left( -\frac{1}{3} \frac{\partial}{\partial t} + a_x \frac{\partial}{\partial x} + a_y \frac{\partial}{\partial y} \right) u_0^{n+1}$$

$$- \frac{1}{2} \frac{\Delta x \Delta y^2}{a_y} \left( 0 \frac{\partial^2}{\partial t^2} + a_x^2 \frac{\partial^2}{\partial x^2} + a_y^2 \frac{\partial^2}{\partial y^2} + a_x \frac{\partial^2}{\partial t \partial x} + a_y \frac{\partial^2}{\partial t \partial y} + 2a_x a_y \frac{\partial^2}{\partial x \partial y} \right) u_0^{n+1} + O(\Delta t^3, \Delta x^3, \Delta y^3)$$

--(a)

From the governing equation,

$$\frac{\partial u}{\partial t} + a_x \frac{\partial u}{\partial x} + a_y \frac{\partial u}{\partial y} = 0 \quad --(b)$$

$$\frac{\partial u}{\partial t} = -a_x \frac{\partial u}{\partial x} - a_y \frac{\partial u}{\partial y}$$



$$\left( \frac{\partial}{\partial t} \right) u = \left( -a_x \frac{\partial}{\partial x} - a_y \frac{\partial}{\partial y} \right) u$$

Apply this operator on  $\frac{\partial u}{\partial x}$

$$\left( \frac{\partial}{\partial t} \right) \frac{\partial u}{\partial x} = \left( -a_x \frac{\partial}{\partial x} - a_y \frac{\partial}{\partial y} \right) \frac{\partial u}{\partial x}$$

$$\frac{\partial^2 u}{\partial t \partial x} = -a_x \frac{\partial^2 u}{\partial x^2} - a_y \frac{\partial^2 u}{\partial y \partial x}$$

$$a_x \frac{\partial^2 u}{\partial t \partial x} = -a_x^2 \frac{\partial^2 u}{\partial x^2} - a_x a_y \frac{\partial^2 u}{\partial y \partial x}$$



Apply this operator on  $\frac{\partial u}{\partial y}$

$$\left( \frac{\partial}{\partial t} \right) \frac{\partial u}{\partial y} = \left( -a_x \frac{\partial}{\partial x} - a_y \frac{\partial}{\partial y} \right) \frac{\partial u}{\partial y}$$

$$\frac{\partial^2 u}{\partial t \partial y} = -a_x \frac{\partial^2 u}{\partial x \partial y} - a_y \frac{\partial^2 u}{\partial y^2}$$

$$a_y \frac{\partial^2 u}{\partial t \partial y} = -a_x a_y \frac{\partial^2 u}{\partial x \partial y} - a_y^2 \frac{\partial^2 u}{\partial y^2}$$

$$a_x \frac{\partial^2 u}{\partial t \partial x} + a_y \frac{\partial^2 u}{\partial t \partial y} = -a_x^2 \frac{\partial^2 u}{\partial x^2} - 2a_x a_y \frac{\partial^2 u}{\partial y \partial x} - a_y^2 \frac{\partial^2 u}{\partial y^2} \quad --(c)$$

In the last expression, we have used the property of

$$\frac{\partial^2 u}{\partial x \partial y} = \frac{\partial^2 u}{\partial y \partial x}$$

which holds if and only if  $u(x, y)$  is *smooth* and *continuous*.

Substitute equations (b) and (c) into (a), one yields

$$\sum_{T \in \cup \Delta_i} (\psi_i^T + \phi_i^T)^{n+1} = -\frac{4\Delta x \Delta y}{3} \frac{\partial u_0^{n+1}}{\partial t} + O(\Delta t^3, \Delta x^3, \Delta y^3)$$

The appearance of the  $-\frac{4\Delta x \Delta y}{3} \frac{\partial u_0^{n+1}}{\partial t}$  term is the main reason on why the method fails to behave third-order-accurate in space for unsteady problem.